# A Non-Hydrostatic Model Using Isentropic Coordinates

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The basic equations in height coordinates

The basic equations in height coordinates, without rotation and friction, are

$$\frac{D\mathbf{V}_{h}}{Dt} = -\frac{1}{\rho} \nabla_{z} p , \qquad (1)$$

$$\frac{Dw}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g , \qquad (2)$$

$$\left(\frac{\partial \rho}{\partial t}\right)_{z} + \nabla_{z} \cdot (\rho \mathbf{V}_{h}) + \frac{\partial}{\partial z} (\rho w) = 0 , \qquad (3)$$

$$\hat{\rho} = \frac{D\theta}{\rho} = Q$$

 $\dot{\theta} \equiv \frac{D\theta}{Dt} = \frac{Q}{\Pi} \,. \tag{4}$ 

Here  $\frac{D}{Dt}$  is the Lagrangian time derivative,  $\mathbf{V}_h$  is the horizontal velocity,  $\rho$  is density, p is pressure, z is height,  $w \equiv \frac{Dz}{Dt}$  is the vertical velocity, g is the acceleration of gravity,  $\theta$  is the potential temperature, Q is the heating rate per unit mass, and  $\Pi$  is the Exner function, which satisfies

$$c_p T = \Pi \theta ,$$

(5)

where  $c_p$  is the heat capacity of air at constant pressure, T is temperature, and

 $\Pi = c_p \left(\frac{p}{p_0}\right)^{\kappa},$ 

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and R is the specific gas constant. Finally, we include the prognostic equation for an arbitrary scalar A, which is

 $\kappa \equiv \frac{R}{c_n},$ 

$$\left[\frac{\partial}{\partial t}(\rho A)\right]_{z} + \nabla_{z} \cdot (\rho \mathbf{V}_{h} A) + \frac{\partial}{\partial z}(\rho w A) = \rho S_{A},$$
(8)

where  $S_A$  is the source of A per unit mass. Finally, we will need the ideal gas law, which is

$$p = \rho RT .$$
(9)

### Transformation to $\theta$ -coordinates

As shown in the *QuickStudy* on coordinate transformations, the horizontal pressure gradient can be transformed to isentropic coordinates as follows:

$$\frac{1}{\rho}\nabla_{z}p = \frac{1}{\rho}\nabla_{\theta}p - \frac{1}{\rho}\frac{\partial p}{\partial z}\nabla_{\theta}z .$$
(10)

The first term on the right-hand side of (10) can be rewritten as follows, using (5), (6), (7) and (9):

(6)

(7)

$$\frac{1}{\rho} \nabla_{\theta} p = RT \frac{\nabla_{\theta} p}{p}$$

$$= \frac{RT}{\kappa} \frac{\nabla_{\theta} \Pi}{\Pi}$$

$$= \frac{c_p T}{\Pi} \nabla_{\theta} \Pi$$

$$= \theta \nabla_{\theta} \Pi$$

$$= \nabla_{\theta} (\Pi \theta)$$

$$= \nabla_{\theta} (c_p T)$$

$$= \nabla_{\theta} s - g \nabla_{\theta} z,$$
(11)

where

$$s \equiv c_p T + gz$$
(12)

Is the Montgomery potential, also known as the dry static energy. Similarly, we write minus the vertical pressure-gradient force as

$$\frac{1}{\rho} \frac{\partial p}{\partial z} = \frac{RT}{p} \frac{\partial p}{\partial z}$$
$$= \frac{RT}{\kappa \Pi} \frac{\partial \Pi}{\partial z}$$
$$= \frac{c_p T}{\Pi} \frac{\partial \Pi}{\partial z}$$
$$= \theta \frac{\partial \Pi}{\partial z}$$
$$= \frac{\partial}{\partial z} (\Pi \theta) - \Pi \frac{\partial \theta}{\partial z}$$
$$= \frac{\partial}{\partial z} (c_p T) - \Pi \frac{\partial \theta}{\partial z}$$
$$= \frac{\partial s}{\partial z} - g - \Pi \frac{\partial \theta}{\partial z}$$
$$= \frac{\partial \theta}{\partial z} \left( \frac{\partial s}{\partial \theta} - \Pi \right) - g .$$

(13)

Using (11) and (13) in (10), we find that

$$\frac{1}{\rho} \nabla_z p = \left( \nabla_\theta s - g \nabla_\theta z \right) - \left[ \frac{\partial \theta}{\partial z} \left( \frac{\partial s}{\partial \theta} - \Pi \right) - g \right] \nabla_\theta z$$
$$= \nabla_\theta s - \frac{\partial \theta}{\partial z} \left( \frac{\partial s}{\partial \theta} - \Pi \right) \nabla_\theta z .$$
(14)

From (13), we see that the hydrostatic equation can be expressed as

$$\frac{\partial s}{\partial \theta} - \Pi = 0 .$$
(15)

Eq. (14) shows that in the hydrostatic limit the horizontal pressure-gradient force is a gradient, when expressed in  $\theta$ -coordinates.

With the use of (13) and (14), we can now rewrite (1) and (2) as

$$\frac{D\mathbf{V}_{h}}{Dt} = -\left[\nabla_{\theta}s - \frac{\partial\theta}{\partial z}\left(\frac{\partial s}{\partial \theta} - \Pi\right)\nabla_{\theta}z\right],\tag{16}$$
$$\frac{Dw}{Dt} = -\frac{\partial\theta}{\partial z}\left(\frac{\partial s}{\partial \theta} - \Pi\right).\tag{17}$$

Using methods discussed in the *QuickStudy* on coordinate transformations, the continuity equation, (3), can be written as

$$\left(\frac{\partial\rho}{\partial t}\right)_{\theta} - \frac{\partial\theta}{\partial z}\frac{\partial\rho}{\partial\theta}\left(\frac{\partial z}{\partial t}\right)_{\theta} + \nabla_{\theta} \cdot (\rho \mathbf{V}_{h}) - \frac{\partial\theta}{\partial z}\left[\frac{\partial}{\partial\theta}(\rho \mathbf{V}_{h})\right] \cdot \nabla_{\theta}z + \frac{\partial\theta}{\partial z}\frac{\partial}{\partial\theta}(\rho w) = 0,$$
(18)

or

$$\frac{\partial z}{\partial \theta} \left( \frac{\partial \rho}{\partial t} \right)_{\theta} - \frac{\partial \rho}{\partial \theta} \left( \frac{\partial z}{\partial t} \right)_{\theta} + \nabla_{\theta} \cdot (\rho \mathbf{V}_{h}) - \left[ \frac{\partial}{\partial \theta} (\rho \mathbf{V}_{h}) \right] \cdot \nabla_{\theta} z + \frac{\partial}{\partial \theta} (\rho w) = 0.$$
(19)

Note that

$$\left[\frac{\partial}{\partial t}\left(\rho\frac{\partial z}{\partial\theta}\right)\right]_{\theta} = \frac{\partial z}{\partial\theta}\left(\frac{\partial\rho}{\partial t}\right)_{\theta} + \rho\frac{\partial}{\partial\theta}\left(\frac{\partial z}{\partial t}\right)_{\theta},$$

(20)

and

$$\nabla_{\theta} \cdot (\rho \frac{\partial z}{\partial \theta} \mathbf{V}_{h}) = \frac{\partial z}{\partial \theta} \nabla_{\theta} \cdot (\rho \mathbf{V}_{h}) + \rho \mathbf{V}_{h} \cdot \nabla_{\theta} \left(\frac{\partial z}{\partial \theta}\right).$$
(21)

Substituting (20) and (21) into (19), we obtain

$$\left(\frac{\partial \rho_{\theta}}{\partial t}\right)_{\theta} + \nabla_{\theta} \cdot \left(\rho_{\theta} \mathbf{V}_{h}\right) - \frac{\partial}{\partial \theta} \left\{ \rho \left[ \left(\frac{\partial z}{\partial t}\right)_{\theta} + \mathbf{V}_{h} \cdot \nabla_{\theta} z - w \right] \right\} = 0 , \qquad (22)$$

where

$$\rho_{\theta} \equiv \rho \frac{\partial z}{\partial \theta}$$

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is the pseudo-density. We recognize

$$\mu \equiv -\rho \left[ \left( \frac{\partial z}{\partial t} \right)_{\theta} + \mathbf{V}_{h} \cdot \nabla_{\theta} z - w \right]$$
(24)

as the upward mass flux across an isentropic surface. This allows us to rewrite (22) as

$$\left(\frac{\partial \rho_{\theta}}{\partial t}\right)_{\theta} + \nabla_{\theta} \cdot \left(\rho_{\theta} \mathbf{V}_{h}\right) + \frac{\partial \mu}{\partial \theta} = 0.$$
(25)

In a similar way, the conservation equation for an intensive scalar, (8), becomes

$$\left[\frac{\partial}{\partial t}(\rho_{\theta}A)\right]_{\theta} + \nabla_{\theta} \cdot (\rho_{\theta}\mathbf{V}_{h}A) + \frac{\partial}{\partial\theta}(\mu A) = \rho_{\theta}S_{A}.$$
(26)

The advective form can be obtained by combining (26) with (25):

$$\left(\frac{\partial A}{\partial t}\right)_{\theta} + \mathbf{V}_{h} \cdot \nabla_{\theta} A + \frac{\mu}{\rho_{\theta}} \frac{\partial A}{\partial \theta} = S_{A} \,.$$
(27)

As a special case of (27), the advective form of the potential temperature equation is

$$\mu = \rho_{\theta} \dot{\theta} \,,$$

(28)

where we have used  $\dot{\theta} \equiv S_{\theta}$ . By using (28), we can rewrite (26) as

$$\left[\frac{\partial}{\partial t}(\rho_{\theta}A)\right]_{\theta} + \nabla_{\theta} \cdot (\rho_{\theta}\mathbf{V}_{h}A) + \frac{\partial}{\partial\theta}(\rho_{\theta}\dot{\theta}A) = \rho_{\theta}S_{A}.$$
(29)

The total time derivative is given by

$$\frac{D}{Dt}(\ ) = \left(\frac{\partial}{\partial t}\right)_{\theta}(\ ) + \mathbf{V}_{h} \cdot \nabla_{\theta}(\ ) + \dot{\theta}\frac{\partial}{\partial \theta}(\ ).$$
(30)

### Summary of the nonhydrostatic equations in $\theta$ -coordinates

The prognostic equations needed to describe non-hydrostatic motions in  $\theta$  -coordinates can now be summarized as follows:

$$\frac{D\mathbf{V}_{h}}{Dt} = -\left[\nabla_{\theta}s - \frac{\partial\theta}{\partial z}\left(\frac{\partial s}{\partial \theta} - \Pi\right)\nabla_{\theta}z\right],$$
(31)
$$\frac{Dw}{Dt} = -\frac{\partial\theta}{\partial z}\left(\frac{\partial s}{\partial \theta} - \Pi\right),$$
(32)
$$\left[\left(\frac{\partial\rho_{\theta}}{\partial t}\right)_{\theta} + \nabla_{\theta}\cdot\left(\rho_{\theta}\mathbf{V}_{h}\right) + \frac{\partial}{\partial\theta}\left(\rho_{\theta}\dot{\theta}\right) = 0\right],$$
(33)
$$\left[\left(\frac{\partial z}{\partial t}\right)_{\theta} = -\mathbf{V}_{h}\cdot\nabla_{\theta}z + w - \frac{\partial z}{\partial\theta}\dot{\theta}\right],$$

(34)

$$\left[\frac{\partial}{\partial t}(\rho_{\theta}A)\right]_{\theta} + \nabla_{\theta} \cdot (\rho_{\theta}\mathbf{V}_{h}A) + \frac{\partial}{\partial\theta}(\rho_{\theta}\dot{\theta}A) = \rho_{\theta}S_{A}.$$

(35)

Not counting the scalar A, the prognostic variables of the  $\theta$ -coordinate model are  $\mathbf{V}_h$ , w,  $\rho_{\theta}$ , and z. The corresponding prognostic variables of the z-coordinate model are  $\mathbf{V}_h$ , w,  $\rho$ , and  $\theta$ .

Finally, we have to determine  $\Pi$ . From  $\rho_{\theta}$  and  $z(\theta)$ , we can find the density  $\rho$ . Then the equation of state in the form

$$\Pi = c_p \left(\frac{\rho R\theta}{p_0}\right)^{\frac{\kappa}{1-\kappa}}$$

(36)

can be used to diagnose  $\Pi$ .

#### The quasi-static limit

In the quasi-static limit, the equation of vertical motion, (32), reduces to the hydrostatic equation in the form

$$\frac{\partial s}{\partial \theta} - \Pi = 0 , \qquad (37)$$

and Eq. (23) for the pseudo-density can be rewritten as

$$\rho_{\theta} = -\frac{1}{g} \frac{\partial p}{\partial \theta}.$$

(38)

To obtain (38) we have used the hydrostatic equation in the form

$$\frac{\partial p}{\partial z} = -\rho g . \tag{39}$$

Even in the quasi-static limit, the pseudo-density is still predicted using (33). Using the known value of the pseudo-density, we can vertically integrate (38) to obtain the pressure and  $\Pi$  as functions of  $\theta$ . We can then use (36) to determine  $\rho$  as a function of  $\theta$ . Finally, we use (39) to compute the height of each  $\theta$  surface, so that (34) is not needed and should not be used. The procedure outlined above can be streamlined somewhat.

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